# **CAD and Finite Element Analysis**

- Most ME CAD applications require a FEA in one or more areas:
  - Stress Analysis
  - Thermal Analysis
  - **Structural Dynamics**
  - Computational Fluid Dynamics (CFD)
  - Electromagnetics Analysis

- ...

- Select verification tools
  - analytic, experimental, other fe method, etc.
- Select element type(s) and degree
  - 3-D solid, axisymmetric solid, thick surface, thin surface, thick curve, thin curve, etc.
- Understand primary variables (PV)
  - Statics: displacements & (maybe) rotations
  - Thermal: temperature
  - CDF: velocity & pressure

- Understand source (load) items
  - Statics: point, line, surface, and volume forces
  - Thermal: point, line, surface, and volume heat generation
- Understand secondary variables (SV)
  - Statics: strains, stresses, failure criterion, error
  - Thermal: heat flux, error

- Understand boundary conditions (BC)
  - Essential BC (on PV)
    - Statics: displacement and/or (maybe) rotation
    - Thermal: temperature
  - Natural BC (on SV)
    - Statics: null surface traction vector
    - Thermal: null normal heat flux
- One or the other at a boundary point.

- Understand reactions at Essential BC
  - Statics:
    - Force at given displacement
    - Moment at given rotation (if active)
  - Thermal:
    - Heat flux at given temperature

- 1. Estimate the solution
- 2. Select an acceptable error (1 %)
- 3. Mesh the model
- 4. Solve the model (PV), post-process (SV)
- 5. Estimate the error
  - A. Unacceptable error: Adapt mesh, go to 3
  - B. Acceptable error: Validate the analysis

#### FE Mesh (FEM)

- Crude meshes that "look like" a part are ok for mass properties but not for FEA.
- Local error is proportional to product of the local mesh size (h) and the gradient of the secondary variables.
- PV piecewise continuous polynomials of degree p, and SV are discontinuous polynomials of degree (p-1).

### **FEA Stress Models**

- **3-D Solid, PV: 3 displacements (no rotations), SV: 6 stresses**
- 2-D Approximations
  - Plane Stress ( $\sigma_{zz} = 0$ ) PV: 2 displacements, SV: 3 stresses
  - Plane Strain ( $\epsilon_{zz} = 0$ ) PV: 2 displacements, SV: 3 stresses (and  $\sigma_{zz}$ )
  - Axisymmetric  $(\partial/\partial \theta = 0)$  PV: 2 displacements, SV: 4 stresses

#### FEA Stress Models, 2

- 2-D Approximations
  - Thick Shells, PV: 3 displacements (no rotations), SV: 5 (or 6) stresses
  - Thin Shells, PV: 3 displacements and 3 rotations, SV: 5 stresses (each at top, middle, and bottom surfaces)
  - Plate bending PV: normal displacement, inplane rotation vector, SV: 3 stresses (each at top, middle, and bottom surfaces)

### FEA Stress Models, 3

- 1-D Approximations
  - Bars (Trusses), PV: 3 displacements (1 local displacement), SV: 1 axial stress
  - Torsion member, PV: 3 rotations (1 local rotation), SV: 1 torsional stress
  - Beams (Frames), PV: 3 displacements, 3
    rotations, SV: local bending and shear stress
    - Thick beam, thin beam, curved beam
    - Pipe element, pipe elbow, pipe tee

#### **FEA Accuracy**

- PV are most accurate at the mesh nodes.
- SV are least accurate at the mesh nodes.
  - (SV are most accurate at the Gauss points)
  - SV can be post-processed for accurate nodal values (and error estimates)

#### **Local Error**

- The error at a (non-singular) point is the product of the element size, h, the gradient of the secondary variables, and a constant dependent on the domain shape and boundary conditions.
  - Large gradient points need small h
  - Small gradient points can have large h
- Plan local mesh size with engineering judgement.

#### **Error Estimators**

- Global and element error estimates are often available from mathematical norms of the secondary variables. The energy norm is the most common.
- It is proven to be asymptotically exact for elliptical problems.
- Typically want less than 1 % error.

#### **Error Estimates**

- Quite good for elliptic problems (thermal, elasticity, ideal flow), Navier-Stokes, etc.
- Can predict the new mesh size needed to reach the required accuracy.
- Can predict needed polynomial degree.
- Require second post-processing pass for localized (element level) smoothing.

# **Primary FEA Assumptions**

- Model geometry
- Material Properties
  - Failure Criterion, Factor of safety
- Mesh(s)
  - Element type, size, degree
- Source (Load) Cases
  - Combined cases, Factors of safety, Coord. Sys.
- Boundary conditions
  - Coordinate system(s)

## **Primary FEA Matrix Costs**

- Assume sparse banded linear algebra system of E equations, with a half-bandwidth of B. Full system if B = E.
  - Storage required, S = B \* E (Mb)
  - Solution Cost, C  $\alpha$  B \* E<sup>2</sup> (time)
  - Half symmetry:  $B \leftarrow B/2$ ,  $E \leftarrow E/2$ ,  $S \leftarrow S/4$ ,  $C \leftarrow C/8$
  - Quarter symmetry: B  $\leftarrow$  B/4, E  $\leftarrow$  E/4, S  $\leftarrow$  S/16, C  $\leftarrow$  C/64
  - Eighth symmetry, Cyclic symmetry, …

## **Symmetry and Anti-symmetry**

- Use symmetry states for the maximum accuracy at the least cost in stress and thermal problems.
- Cut the object with symmetry planes (or surfaces) and apply new boundary conditions (EBC or NBC) to account for the removed material.

## Symmetry (Anti-symmetry)

- Requires symmetry of the geometry and material properties.
- Requires symmetry (anti-symmetry) of the source terms.
- Requires symmetry (anti-symmetry) of the essential boundary conditions.

## **Structural Model**

- Symmetry
  - Zero displacement normal to surface
  - Zero rotation vector tangent to surface
- Anti-symmetry
  - Zero displacement vector tangent to surface
  - Zero rotation normal to surface

## **Thermal Model**

- Symmetry
  - Zero gradient normal to surface (insulated surface, zero heat flux)
- Anti-symmetry
  - Average temperature on surface known

#### **Local Singularities**

• All elliptical problems have local radial gradient singularities near re-entrant corners in the domain.  $u = r^{p} f(\theta)$  $\partial u/\partial r = r^{(p-1)} f(\theta)$ 



Corner: p = 2/3, weak

Crack: p = 1/2, strong

 $\partial u/\partial r \Rightarrow \infty \text{ as } r \Rightarrow 0$ 

- Prepare initial estimates of deflections, reactions and stresses.
- Eyeball check the deflected shape and the principal stress vectors.

- The stresses often depend only on the shape of the part and are independent of the material properties.
- You must also verify the displacements which almost always depend on the material properties.

- The reaction resultant forces and/or moments are equal and opposite to the actual applied loading.
- For pressures or tractions remember to compare their integral (resultant) to the solution reactions.
- Reactions can be obtained at elements too.

- Compare displacements, reactions and stresses to initial estimates. Investigate any differences.
- Check maximum error estimates, if available in the code.

- Prepare initial estimates of the temperatures, reaction flux, and heat flux vectors.
- Eyeball check the temperature contours and the heat flux vectors.
- Temperature contours should be perpendicular to an insulated boundary.

- The temperatures often depend only on the shape of the part.
- Verify the heat flux magnitudes which almost always depend on the material properties.

- The reaction resultant nodal heat fluxes are equal and opposite to the applied heat fluxes.
- For distributed heat fluxes remember to compare their integral (resultant) to the solution reactions.
- Reactions can be obtained at elements too.

- Compare temperatures, reactions and heat flux vectors to initial estimates. Investigate any differences.
- Check maximum error estimates, if available in the code.